

EXPERIMENTAL AND NUMERICAL SOLUTIONS OF CONTACT FATIGUE

K. Frydryšek*, J. Lenert*, L. Václavek*, J. Fuxa*, R. Halama*

Summary: *This article shows:*

1. Some studies of a low-cycle material fatigue caused by cyclical contact between two spheres with the same diameters. The spheres are made up from modified 15219 steel. The problem was solved by FEM (SW MSC.MARC/Mentat. The results show hysteresis loops from which the number of cycles until fracture can be determined.

2. The realisation of test device for the research of contact fatigue as complement of the loading test machine INOVA, which is directed to look for quantitative coherence between number of cycles to the origin of fatigue cracks in the area of mechanical contact.

1. Introduction

For material failures that are caused by the low-cycle fatigue (LCF), it is necessary to describe material behaviour using a closed hysteresis loop (an area of cyclical plasticity). To determine the lifetime of machine parts it is important to find the total number of cycles which cause the initialisation of first fatigue cracks. This paper describes some case of LCF study for the mechanical cyclical contact between two spheres with the same diameters. Material behaviours were acquired from experiments. The test machine for the research of contact fatigue as a complement of the servo-hydraulic machine INOVA 200kN is shown in fig.4. This machine was proposed and realised in the department of mechanics of Materials at VŠB – TECHNICAL University of Ostrava.

2. The Numerical Solution

The basic boundary conditions are the axi-symmetric condition (around the X-axis) and the planar symmetry (YZ-plane).

*MSc. Karel FRYDRÝŠEK, Ph.D., tel.: +420597324552, fax: +420596916490,
e-mail: karel.frydrysek@vsb.cz;

Prof. MSc. Jiří LENERT, Ph.D., tel.: +420597321232, fax: +420596916490, e-mail: jiri.lenert@vsb.cz;

MSc. Leo VÁCLAVEK, Ph.D., tel.: +420597324555, fax: +420596916490, e-mail: leo.vaclavek@vsb.cz;

Prof. MSc. Jan FUXA, Ph.D., tel.: +420597324412, fax: +420596916490, e-mail: jan.fuxa@vsb.cz;

MSc. Radim HALAMA, tel.: +420597323293, fax: +420596916490, e-mail: radim.halama.fs@vsb.cz;

VŠB – Technical University of Ostrava, Faculty of Mechanical Engineering, Department of Mechanics of Materials, Třída 17. listopadu 15, 708 33, Ostrava-Poruba, Czech Republic.

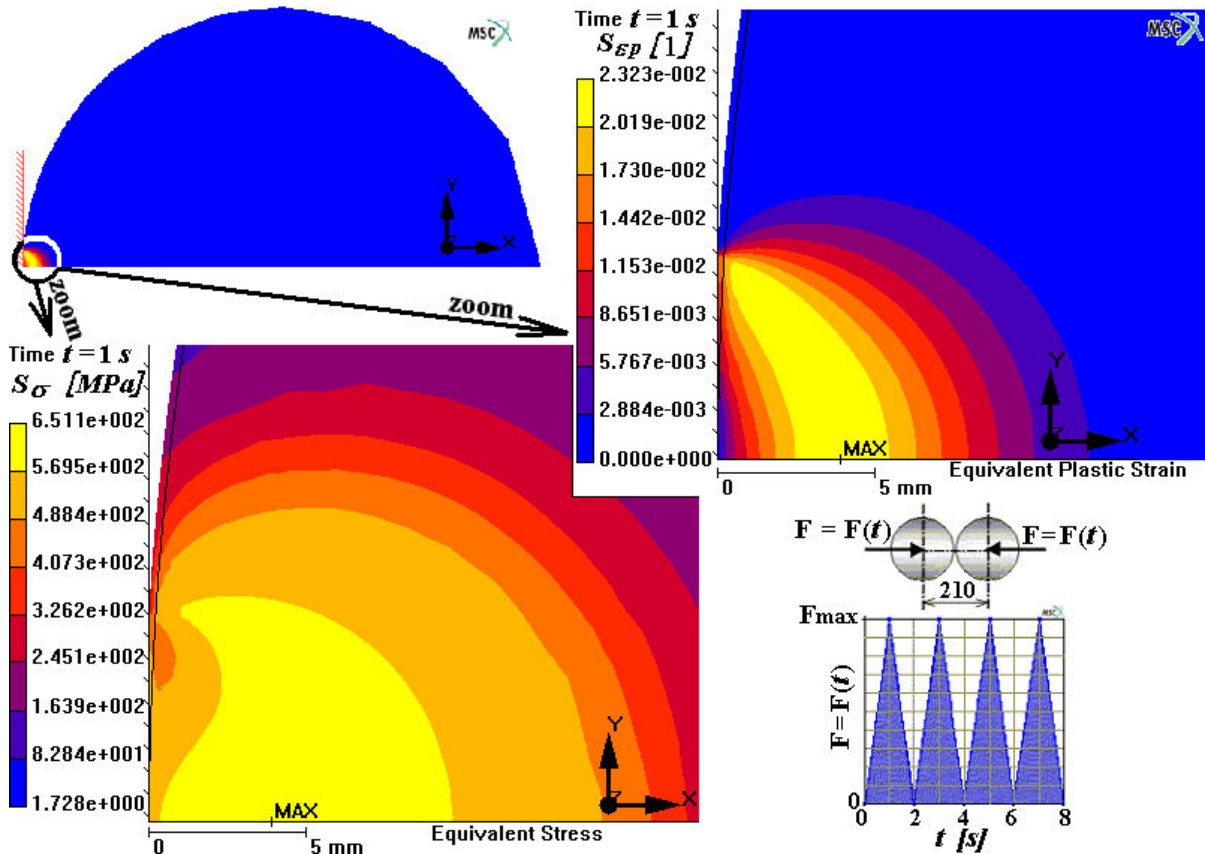


Fig.1 The values of equivalent plastic strain S_{ϵ_p} and equivalent von Mises stress S_{σ} .

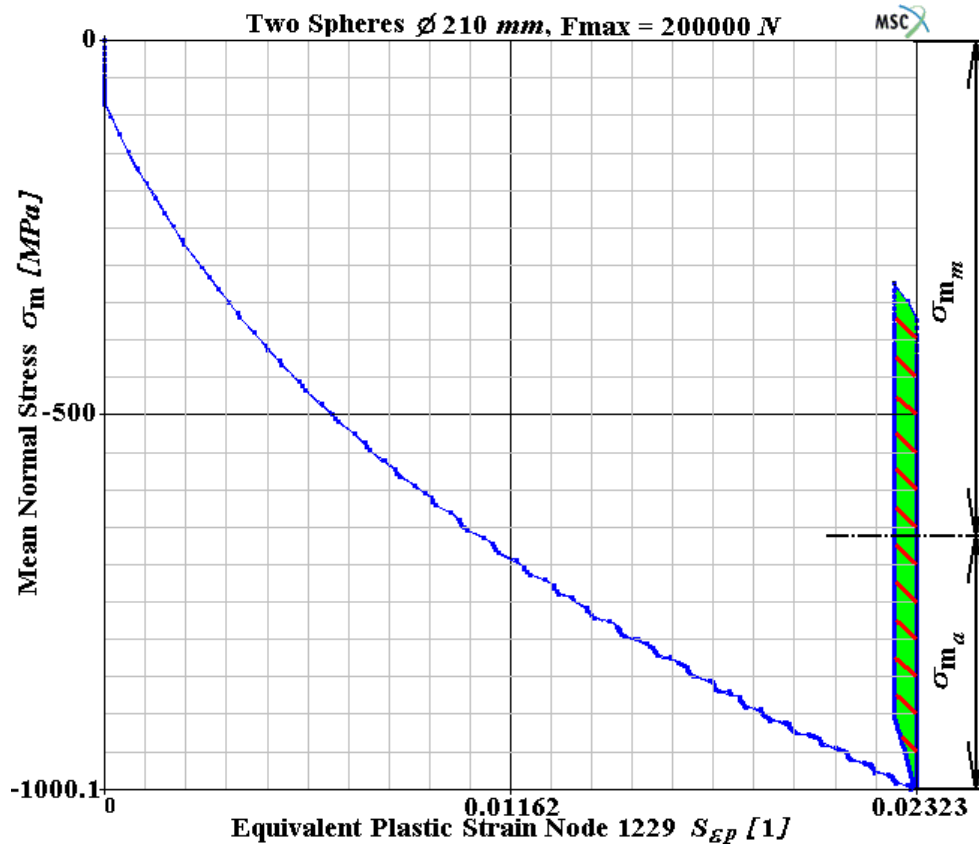


Fig.2 First proposal model of fictive hysteresis loop (S_{ϵ_p} - σ_m dependence).

During the pulse pressing of two identical spheres (with diameter ϕ 210 mm), the contact area must be a circle plane.

Therefore it is advantageous and necessary to solve only one sphere, which is in mechanical contact with the absolutely rigid plane.

A time-dependent periodical force $F=F(t)$ (which contains four cycles with maximum value $F_{max} = 200000\text{ N}$ and minimum value $F_{min} = 0\text{ N}$) acted in the centre of the sphere, see fig.1.

The material is considered to be isotropic and elasto-plastic with kinematic hardening rule, which is sometimes advisable for the LCF phenomenon.

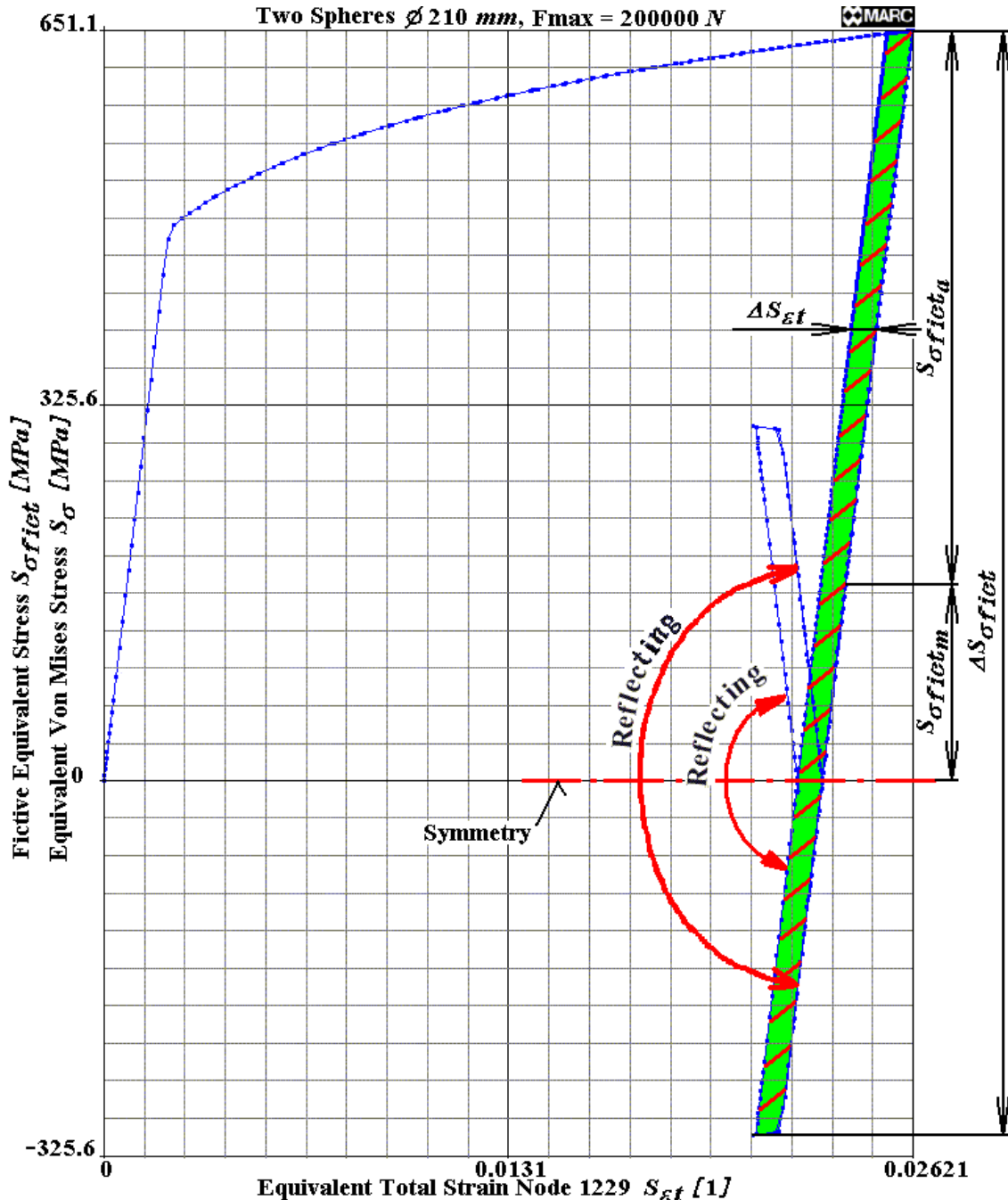


Fig.3 Second proposal model of fictive hysteresis loop. The $S_{\epsilon t} - S_{\sigma}$ and $S_{\epsilon t} - S_{\sigma_{fict}}$ dependencies during the solution.

In this case, the hysteresis loop (equivalent total strain S_{ε_t} [1] - equivalent von Mises stress S_{σ} [MPa] dependence) for the critical point of the material was calculated from FE solution.

The cyclical changing of equivalent plastic strains S_{ε_p} [1], equivalent elastic strains S_{ε_e} [1], equivalent total strains S_{ε_t} [1] and mean normal stresses $\sigma_m = (\sigma_1 + \sigma_2 + \sigma_3)/3$ [MPa] are shown (cyclical plasticity), see fig.2, and 3. At this point it is possible to calculate the number of cycles N_f [cycle] needed for initiation of fatigue cracks.

Hence Fig.2 shows first proposal model of hysteresis loop based on S_{ε_p} - σ_m dependence. This fictive hysteresis loop (shaded area in fig.2) should be important in calculating the number of cycles N_f necessary for fatigue crack initiation via equation:

$$N_f = \frac{1}{2} \left(\frac{\sigma_{m_a}}{\sigma'_f} \right)^{\frac{1}{b}} \left(1 - \frac{\sigma_{m_m}}{\sigma'_f} \right)^{\frac{-1}{b}} \quad (1)$$

where σ'_f [MPa] and b [1] are material parameters.

Figure 3 shows second proposal model of fictive hysteresis loop (S_{ε_t} - $S_{\sigma_{fict}}$ dependence) based on the (S_{ε_t} - S_{σ} dependence), where $S_{\sigma_{fict}}$ is a fictive equivalent stress measured in [MPa]. This fictive hysteresis loop (shaded area in fig.3) probably should be important in calculating the number of cycles N_f necessary for fatigue crack initiation. The fictive loop was created by reflecting of some parts S_{ε_t} - S_{σ} dependence about the axis of symmetry. This axis of symmetry is defined via values where $S_{\sigma} = 0$ MPa.

The number of cycles N_f with consideration of mean and amplitude stresses can be calculated using the following equation.

$$N_f = \frac{1}{2} \left(\frac{S_{\sigma_{fict_a}}}{\sigma'_f} \right)^{\frac{1}{b}} \left(1 - \frac{S_{\sigma_{fict_m}}}{\sigma'_f} \right)^{\frac{-1}{b}}. \quad (2)$$

3. Realisation of Test Machine for the Research of Contact Fatigue

The test machine for the research of contact fatigue as a complement of the servo-hydraulic machine INOVA 200kN is shown in fig.4. This machine was proposed and realised in the department of mechanics of Materials at VŠB – TECHNICAL University of Ostrava.

This machine will be used:

1. for the solution of quantitative coherence between number of cycles to the origin of fatigue cracks in microstructures of different materials by contact fatigue and number of cycles.

2. for initiation of crack by combination of tensile and pressure stresses in the area of the fatigue of materials.
 3. The experimental results will be also important for future numerical solutions
- For more details see [2] and [3].

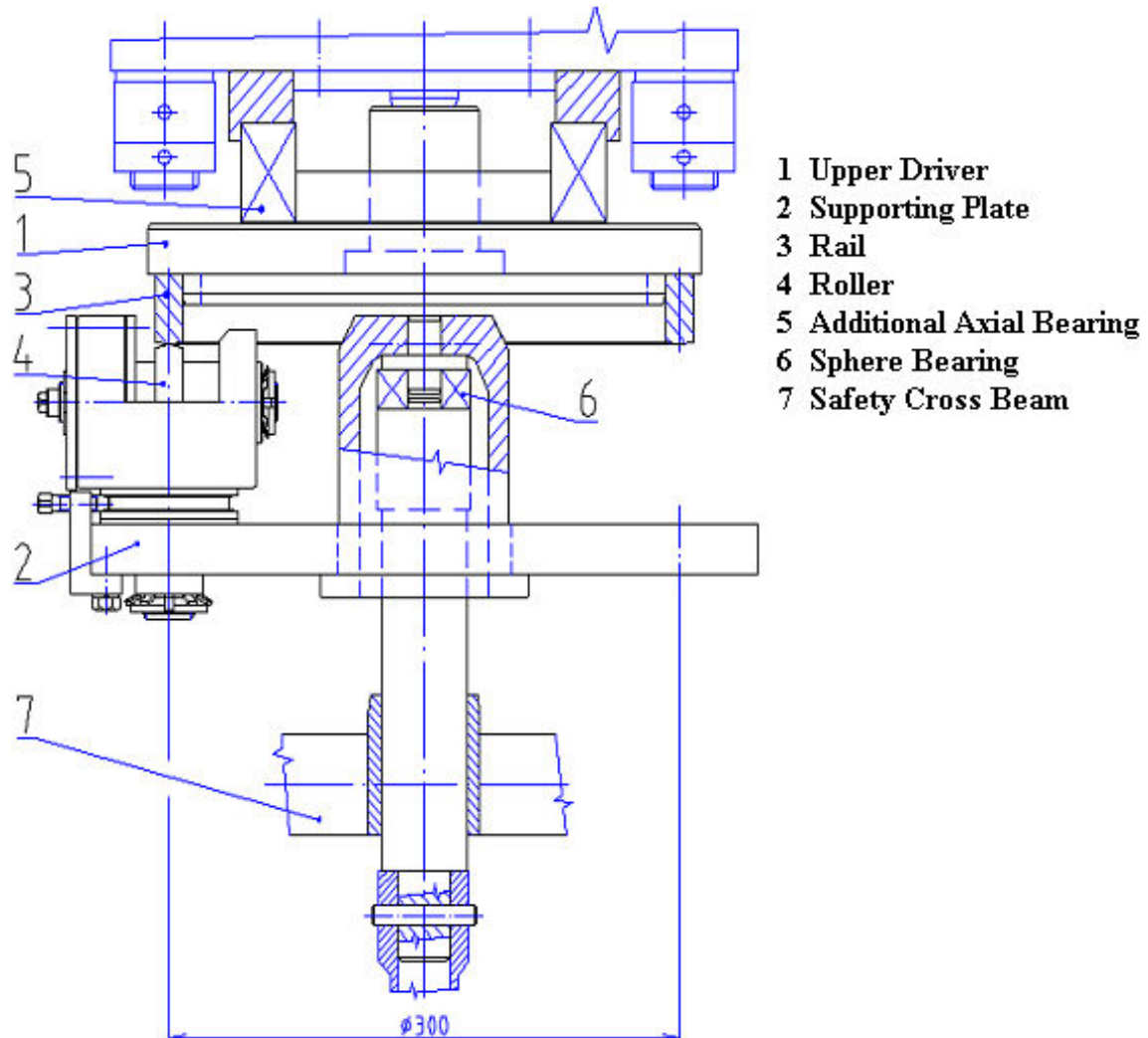


Fig.4 Diagram of the machine for contact fatigue tests.

CONCLUSIONS

By FE simulations of twin spheres with the same diameters, which follow the kinematic hardening rule, it is possible to solve LCF problems. Figure 2 and 3 show the hysteresis loop and fictive hysteresis loop, which are important for calculation of the number of cycles necessary for fatigue crack initiation. Equation (1) or (2) describes one possible way of calculating the number of cycles N_f . This numerical study is good base for future experimental measurements in our department. This paper and the given references show that the FE model can be used to simulate plastic shakedown and ratchetting material responses but experiments are necessary.

The test machine for the research of contact fatigue as complement of the loading test machine INOVA was realised.

This work has been funded by the Czech projects MSM 272300009.

REFERENCES

- [1] LENERT, J., FRYDRÝŠEK, K., VÁCLAVEK, L., KUČERA, J., HALAMA, R.: Závěrečná zpráva výzkumného záměru č. J17/98: 272 300009, Zvyšování provozní spolehlivosti strojů a strojní zařízení a snižování jejich negativních vlivů na životní prostředí (Dílčí část 8 - Únavová životnost v kontaktní únavě), FS VŠB-TU Ostrava, katedra pružnosti a pevnosti, Ostrava 2002.
- [2] LENERT, J., FUXA, J., KUČERA, J., VÁCLAVEK, L., FRYDRÝŠEK, K., HALAMA, R., ŠÁREK, L.: Závěrečná zpráva výzkumného záměru č. J17/98: 272 300009, Zvyšování provozní spolehlivosti strojů a strojní zařízení a snižování jejich negativních vlivů na životní prostředí (Dílčí část 7 - Únavová životnost v kontaktní únavě), FS VŠB-TU Ostrava, katedra pružnosti a pevnosti, Ostrava 2002.
- [3] FUXA, J.: Výzkum kritérií únavové pevnosti kvaziizotropního materiálu namáhaného v podmínkách dvojosého napětíového stavu, závěrečná zpráva projektu GAČR 101/99/1245, FS VŠB-TU Ostrava, katedra pružnosti a pevnosti, Ostrava 2001.
- [4] FRYDRÝŠEK, K., VÁCLAVEK, L., KUČERA, J., LENERT, J., ADÁMKOVÁ, L.: Low-cycle Fatigue & Mechanical Contact, In: Sborník 39. mezinárodní konference „Experimentální analýza napětí 2001 - EAN 2001“, Tábor, ČVUT Praha, 2001, ISBN 80-86246-09-4, s. 69-74.
- [5] HALAMA, R., FRYDRÝŠEK, K.: Výpočty kontaktu kladky a kolejnice pomocí MKP, In: WORKSHOP 2003 Fakulty strojní, VŠB-TU Ostrava, ISBN 80-248-0233-3, s. 125-128.