

INFLUENCE OF TISSUE CHANGES IN SUPERFICIAL LAMINA PROPRIA ON PRODUCTION OF CZECH VOWELS

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Abstract: Superficial lamina propria (SLP) is a water-like vocal fold (VF) layer located directly under overlying epithelium. Its material properties affect VF motion and thus resulting spectrum of produced sound. Influence of stiffness and damping of the SLP on sound spectrum of Czech vowels is examined using a twodimensional (2D) finite element (FE) model of a human phonation system. The model consists of the VF (structure model) connected with an idealized trachea and vocal tract (VT) (fluid models). Five VTs for all Czech vowels [a:], [e:], [i:], [o:] and [u:] were used and their geometry were based on MRI data. Fluid flow in the trachea and VT was modelled by unsteady viscous compressible Navier-Stokes equations. Such a formulation enabled numerical simulation of a fluid-structure-acoustic interaction (FSAI). Self-sustained oscillations of the VF were described by a momentum equation including large deformations and a homogeneous linear elastic model of material was used. Fluid and structure solvers exchange displacements and boundary forces in each iteration. During closed phase VFs are in contact and fluid flow is separated. We can observe that both the damping and the stiffness of the SLP substantially influence the amplitude and frequency of VFs vibration as well as the open time of the glottis.

Keywords: Simulation of phonation, Fluid-structure-acoustic interaction, Czech vowels, Finite element method, Biomechanics of voice.

1. Introduction

Changes between convergent and divergent glottal shape play a crucial role in energy transfer during selfsustained oscillations of VFs, see Thomson et al. (2005). Since the structure of VF surface is similar to an inflatable ball filled with water, we can imagine the epithelium as a ball and the SLP as water. Thus tissue changes in the SLP influence self-oscillations of the VFs.

Tanabe et al. (1979) and Chan et al. (2000) measured, modelled and extrapolated damping ratios of selected VF layers, which can be used for FE modelling of VF motion. They showed that VF damping is below a critical damping value with the damping ratio around 0.1. Titze et al. (2017) pointed out that stiffness of the VF is more dominant than tension for oscillation frequencies under 1000 Hz. One of the most recent studies of Zhang (2016) investigated effects of VF thickness of medial surface, glottal opening, subglottal pressure and VF stiffness. He concluded that the increasing stiffness reduces noise and amplifies higher-order harmonics in vowel spectrum to some extent.

The 2D computational model presented in this article continues the previous works of Švancara et al. (2014) and Hájek et al. (2018). The three previous VT shapes for Czech vowels are complemented here by two

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additional VTs for Czech vowels [e:] and [o:] reconstructed from MRI data, see Radolf (2010). Also, the fluid FE mesh was refined here to capture smaller eddies.

2. Methods

All 2D FE models of FSAI during VF self-oscillation were developed in the software ANSYS 15.0, see Fig. 1 a)–e), g). The models consist of simplified trachea, four-layered VF based on M5 geometry, see Scherer et al. (2001), and five VTs for all Czech vowels [a:], [e:], [i:], [o:] and [u:]. All the models are composed of 16 097 linear elements with 16 306 nodes. Material parameters (including damping) are summarized in Fig. 1 f), i).

The computational algorithm is as follows: the model is excited by a mean lung pressure $p_{Lu} = 270 \text{ Pa}$ at the entrance to the trachea (Fig. 1 a)). The air flow propagates through the trachea and loads the VFs which start to move. When VFs open the air flows through the VT and generates pressure waves forming the vowel spectrum. Deformation of the fluid mesh is solved by an in-house Arbitrary-Lagrangian-Eulerian algorithm, details in Švancara et al. (2014).



Fig. 1: a) 2D FE model for the [o:] vowel, b)–e) vocal tracts for the remaining vowels, f) material properties of the fluid model where c_{air} – speed of sound in the air, η – dynamic viscosity and ρ – density, g) fourlayered model of VF, h) four variants of chosen damping ratios and i) material properties of the VF where E – Young's modulus, μ – Poisson's ratio and ρ – density.

Eighty combinations of tested parameters were prepared, see Tab. 1. Four variants of Young's moduli of the SLP (E_{SLP}) were used for each vowel and four variants of damping were used for each stiffness E_{SLP} according to Tab. 1. From pairs of damping ratios b_{p1} and b_{p2} (Fig. 1 h)) and from the natural frequencies of the VF coefficients of proportional damping α and β were calculated and used in computations, for details see Hájek et al. (2018). Each computation of a 0.1 s long phonation took between 7 and 12 hours on Intel® CoreTM i7–7700K with 32 Gb of RAM.

3. Results and discussion

The structural results are given in Tab. 1. Vibration frequency f, maximal width of glottis WG_{max} and open quotient OQ were evaluated from one of the last computed periods, see Fig. 2 (top left). From the results it is apparent that both the increasing stiffness and increasing damping reduce WG_{max} . Rising stiffness also

decreases OQ whereas damping has an opposite influence in some variants. Frequency of self-sustained VF vibrations f lies between 80 and 170 Hz which is in a range of normal male phonation.

E _{SLP} [Pa]	α [s ⁻¹]	β [s]	[a:]			[e:]			[i:]			[0:]			[u:]		
			<i>f</i> [Hz]	WG _{max} [mm]	0Q [-]	<i>f</i> [Hz]	WG _{max} [mm]	<i>OQ</i> [–]	f [Hz]	WG _{max} [mm]	0Q [-]	f [Hz]	WG _{max} [mm]	0Q [-]	<i>f</i> [Hz]	WG _{max} [mm]	0Q [-]
2000	0.5083	0.0002	Comp	omputation crashed		Computation crashed		rashed	Computation crashed			Commutation and bod			Commutation and 1 1		
	1.0165	0.0004	130	0.39	0.26	137	0.48	0.37	141	0.45	0.38	Computation crashed			Computation crashed		
	60.3776	0.0006	130	0.39	0.30	137	0.49	0.41	137	0.43	0.42	135	0.46	0.32	137	0.42	0.33
	119.7386	0.0007	132	0.37	0.33	143	0.46	0.43	133	0.43	0.44	133	0.44	0.33	133	0.41	0.35
2500	1.7917	0.0002	130	0.34	0.22	Comp	utation c	rashed	154	0.38	0.28	139	0.36	0.22	Comp	utation c	rashed
	3.5834	0.0004	115	0.32	0.24	143	0.42	0.36	137	0.38	0.38	132	0.37	0.28	130	0.34	0.30
	64.4495	0.0006	116	0.30	0.27	133	0.39	0.39	133	0.36	0.41	128	0.34	0.31	130	0.34	0.32
	125.3155	0.0007	120	0.30	0.29	135	0.39	0.39	115	0.42	0.32	123	0.32	0.32	125	0.32	0.34
3000	2.7622	0.0002	119	0.29	0.20	169	0.32	0.31	137	0.33	0.30	116	0.28	0.19	112	0.31	0.20
	5.5243	0.0004	128	0.29	0.24	133	0.33	0.28	169	0.27	0.29	130	0.29	0.25	108	0.30	0.23
	67.5990	0.0006	103	0.27	0.23	116	0.29	0.28	106	0.27	0.24	111	0.28	0.26	104	0.28	0.25
	129.6737	0.0007	99	0.26	0.23	118	0.29	0.28	112	0.25	0.27	100	0.28	0.23	122	0.27	0.29
3500	3.5315	0.0002	108	0.23	0.17	119	0.26	0.18	100	0.21	0.14	133	0.25	0.21	116	0.24	0.20
	7.0631	0.0004	85	0.24	0.16	122	0.25	0.26	78	0.24	0.16	106	0.26	0.21	104	0.25	0.21
	70.1592	0.0005	VF did not open		VF did not open			VF	VF did not open			VF did not open			VF did not open		
	133.2553	0.0007	vi uu not open					V I									

Tab. 1: Vibration characteristics of VFs.

Fig. 2 on the right shows the acoustic pressure measured 5 mm below lips from which point the power spectral densities are evaluated. Peaks of flow velocity between VFs occur around the start and end of open phase which we can see in the Fig. 2 (bottom left).



Fig. 2: Example of results for vowel [e:], most damped case with $E_{SLP} = 2000 \text{ Pa}$. Top left: displacement of VFs in mediolateral direction from a node on the left and right VF medial surface (solid line) and from minimal glottal width (dashed line). Bottom left: flow velocity from a node between VFs. Right: acoustic pressure near the lips.

Fig. 3 shows comparison between two spectra of acoustic pressure near the lips for the vowel [o:]. One can observe that the less stiff and more damped SLP (left graph) can generate harmonic peaks near the first and second formant frequency while all the spectral peaks generated by stiffer and less damped SLP (right graph) are lower and flattened. The first two formants lie close together at 550 Hz and 700 Hz. These two formats are in the range measured by Merhaut (1972). Frequency shift was not observed among computed variants.

4. Conclusion

Extensive sensitivity analysis was done to explore the influence of stiffness and damping of SLP on VFs motion and produced sound for all Czech vowels. The developed 2D FE model of a human phonation



Fig. 3: Power spectral densities of acoustic pressure at node near the lips for vowel [0:]. Left: $E_{SLP} = 2000 Pa$ with damping var. 3 according Fig. 1 h). Right $E_{SLP} = 3500 Pa$ with damping var. 1.

enables to use different shapes of VTs and allows changing various model parameters such as stiffness and damping. Results show that varying properties of SLP affect motion of VFs and resulting vibration characteristics. Maximum width of glottis is most affected by these properties. Properties of SLP tissue could vary due to pathology, for instance Reinke's edema.

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